

OXIDATIVE DEGRADATION KINETICS OF RECALCITRANT MACRO AND MICROPOLLUTANTS USING CaMFeO_3 (M = Cu, Mo, Co) PEROVSKITE CATALYST

Understanding the kinetics behavior of recalcitrant organic degradation in presence of catalyst is important in determining the reaction rates of catalysis. Therefore, this study investigates the kinetic behavior of oxidative degradation for different types of recalcitrant organic pollutants, namely as acid orange II (AOII) macropollutant and caffeine (CAF) micropollutant using B-site substituted CaMFeO_3 (M = Cu, Mo, Co) perovskite catalysts. The kinetic study was analyzed based on four kinetic models which are pseudo-zero-order, first-order, second-order and BMG. Interestingly, CaCuFeO_3 exhibited a unique kinetic behavior in which the reaction followed a different kinetic model: pseudo-second-order for AOII and pseudo-first-order for CAF. The reaction rate of CAF degradation in the presence of CaCuFeO_3 was increased by nine orders of magnitude ($k = 1.8 \times 10^{-3} \text{ min}^{-1}$) within 4 hr of reaction compared to pristine CaFeO_3 ($k = 0.2 \times 10^{-3} \text{ min}^{-1}$). On the contrary, CaFeO_3 , CaMoFeO_3 and CaCoFeO_3 were fitted to BMG kinetic model for the CAF degradation. These results indicate that the partial substitution of B-site cation in the perovskite structure alters the catalytic reactivity of the resultant substituted perovskite catalysts and subsequently influences the overall kinetics behavior of the oxidative degradation in both recalcitrant macro and micropollutants.

Keyword: Kinetic; Perovskite Catalyst; B-site Cation; Macropollutant; Micropollutant

1. Introduction

Advanced oxidation processes (AOPs), such as Fenton reactions, photocatalytic oxidation, electrochemical oxidation reactions and ozone oxidation are being recognized as effective methods for wastewater treatment in degrading a wide range of recalcitrant organic pollutants [1,2]. Among all the available AOPs, Fenton oxidation is one of the most extensively utilized AOPs due to its rapid reaction rate and high oxidation capacity. The Fenton oxidation process involves a series of complex reactions with the main reaction of Fe^{2+} with H_2O_2 , producing highly reactive hydroxyl radicals ($\cdot\text{OH}$) (Eq. (1)). When the Fe^{3+} reacts with H_2O_2 , it regenerates into Fe^{2+} and produces hydroperoxyl radicals ($\cdot\text{OOH}$) (Eq. (2)) [3]. Most organic pollutants can be efficiently and non-selectively degraded by $\cdot\text{OH}$ radicals during catalysis due to its high redox potential ($E^o = 2.80 \text{ V}$) [4].



Conventional Fenton oxidation is usually conducted under acidic conditions due to the tendency of Fe^{3+} to precipitate and lose its catalytic efficacy at high pH levels. However, maintaining the pH at acidity region could increase the expense of treatment and negatively impact soil and water quality [5,6]. Therefore, the heterogeneous Fenton/Fenton-like process has garnered significant interest due to its ability to overcome the limitations of the homogeneous Fenton process. In the heterogeneous Fenton/Fenton-like system, the catalytic reactions take place within the vicinity of active sites on the surface of the solid catalyst, avoiding the leaching of iron ions, extending the operating pH range (including natural pH value of water), minimizing the generation of iron sludge and facilitating facile catalyst's recovery [7-9].

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As a result, many heterogeneous Fenton/Fenton-like catalysts have been developed, including metal-organic frameworks [10,11], graphene oxide [12,13] and mixed oxides such as perovskites [14-17], while the latter is typically preferable for environmental heterogeneous catalysis application.

Perovskite (ABO_3) is a type of crystalline ceramic that is classified in a group of mixed oxides. A-site represents an alkaline-earth metals or rare-earth metals, while B-site represents a transition metal. The physiochemical properties of the perovskite can be deliberately tailored by substituting different elements at the A and/or B sites, which are able to modulate the overall catalytic performances for the degradation of organic pollutants. Recent studies have shown that an improvement in catalytic performance as well as degradation kinetics rate was observed when different types of cations in the B-site either partially or fully substituted in the perovskite structure. For instance, Rao et. al. [18] introduced Cu-substituted $LaFeO_3$ ($LaFe_{0.925}Cu_{0.075}O_{3-\delta}$) for sulfadiazine degradation, which showed that substitution of foreign cation into the B-site significantly increased the reaction kinetic constant from 0.0759 min^{-1} for $LaFeO_3$ to 0.3829 min^{-1} for $LaFe_{0.925}Cu_{0.075}O_{3-\delta}$. Meanwhile, Xie et. al. [19] reported that the enhancement of redox activity between Co and Cu in $LaCo_{0.4}Cu_{0.6}O_{3-\delta}$ facilitated the activation of H_2O_2 to HO^\bullet radicals, which led to a complete degradation of ciprofloxacin (CIP) within 2 hr of reaction time. The reaction kinetic constant value of CIP degradation by $LaCo_{0.4}Cu_{0.6}O_{3-\delta}$ ($k = 0.03945 \text{ min}^{-1}$) was 2.5 times higher than that of $LaCoO_3$. Gao et. al. [20] also achieved a complete degradation of sulfamethoxazole over Cu substituted in $LaMnO_3$ and the reaction kinetic constant ($k = 0.2001 \text{ min}^{-1}$) enhanced by 8.3 times as compared to $LaMnO_3$. Based on the above discussions, the degradation of recalcitrant emerging micropollutants by B-site substituted perovskite structure mainly followed the first order reaction kinetic model. Similar behaviors of first order kinetic model by other B-site substituted perovskite catalysts for oxidative degradation of recalcitrant micropollutants were also observed elsewhere [21-23]. Nevertheless, it is necessary to evaluate the impact of partial substitution of B-site cation on the degradation reaction rate constants of organic pollutants using different kinetic models. In-depth understanding of laboratory-scale kinetic models is crucial to gaining detailed insights into chemical reactions, optimizing reaction conditions, and ensuring the safety that warrants efficient and sustainable industrial practice.

Hence, the present work aims to evaluate the oxidative degradation kinetics of recalcitrant macro and micropollutants using $CaMFeO_3$ ($M = Cu, Mo, Co$) perovskite catalysts using different types of kinetic models (pseudo-zero-order, first-order, second-order and BMG-Behnajady, Modirshahla, and Ghanbary). The kinetic study of the macropollutant (acid orange II (AOII)) was performed using data from previous work [15], while caffeine (CAF) was chosen as the model micropollutant because it is considered as the most widely consumed psychoactive drugs globally, with an estimated consumption of about 120,000 tonnes annually [24,25]. CAF is also known as the most frequently detected pharmaceutically active compounds

in the aquatic environment [26], and conventional waste water treatment plants are not able to effectively degrade CAF, which can give adverse effect to human and aquatic life after long-term exposure. The reactivity of $CaMFeO_3$ ($M = Cu, Mo, Co$) perovskite catalysts on CAF degradation and the reaction kinetic models for both AOII macropollutant and CAF micropollutant were discussed in this study.

2. Material and experimental procedure

2.1. Materials

Calcium nitrate tetrahydrate ($Ca(NO_3)_2 \cdot 4H_2O$; $\geq 99\%$), iron(III) nitrate nonahydrate ($Fe(NO_3)_3 \cdot 9H_2O$; 99%), ammonium molybdate ($(NH_4)_2MoO_4$; 99%), cobalt(II) chloride hexahydrate ($CoCl_2 \cdot 6H_2O$; 98%), copper(II) nitrate trihydrate ($Cu(NO_3)_2 \cdot 2.5H_2O$; $\geq 99\%$), ethylenediaminetetraacetic acid (EDTA), ammonium hydroxide (NH_4OH) solution, hydrogen peroxide (H_2O_2 ; 30% (w/w)), acid orange II (AOII), caffeine (CAF) (99%) and methanol for liquid chromatography (LiChrosolv® Reag. Ph Eur; 99%) were supplied by Sigma Aldrich. Citric acid monohydrate ($C_6H_8O_7 \cdot H_2O$; $\geq 99\%$) was purchased from QReC (Asia). All chemicals were of analytical grade and used as received without further purification.

2.2. Synthesis of B-site substituted $CaMFeO_3$ ($M = Mo, Co, Cu$) perovskite catalysts

The series of B-site substituted $CaMFeO_3$ ($M = Mo, Co, Cu$) perovskites was synthesized via EDTA-citric acid complexation method. Each A-site and B-site cation molar concentration was fixed at 0.05 M. A set of molar ratios of A-site precursor: B'-site precursor: B-site precursor: ethylenediamine tetra-acetic acid (EDTA): citric acid: ammonium hydroxide was kept constant at 1:1:1:1.1:2:10. For instance, in the synthesis of $CaMoFeO_3$ catalyst, 0.05 M $Ca(NO_3)_2 \cdot 4H_2O$, 0.05 M $FeCl_3 \cdot 6H_2O$, 0.05 M $(NH_4)_2MoO_4$ and 0.1 M $C_6H_8O_7 \cdot H_2O$ solutions were mixed and stirred for 15 min at the beginning. Then, a solution mixture containing 0.05 M NH_4OH and 0.055 M EDTA was added to the former mixture and stirred for 15 min at room temperature until well mixed.

Subsequently, the resultant homogeneous mixture was heated at $100^\circ C$ under stirring to evaporate water to form a viscous solution. Further gelation of the viscous solution was carried out in the oven at $90^\circ C$ for 24 hr. The dried gel samples then underwent a two-stage calcination process in a muffle furnace: first stage at $450^\circ C$ for 8 h and second stage at $800^\circ C$ for 4 h at a ramping rate of $5^\circ C \text{ min}^{-1}$ in air. The resultant $CaMoFeO_3$ perovskite was ground and stored prior to further use. Similar procedures were repeated for other B-site substituted perovskite catalysts using copper and cobalt precursors to synthesize $CaCuFeO_3$ and $CaCoFeO_3$, respectively. In addition, $CaFeO_3$ was also synthesized as a pristine unsubstituted B-site catalyst for comparison purposes.

2.3. Catalytic performances and kinetic analysis

The catalytic activities of the B-site substituted CaMFeO_3 perovskite catalysts were evaluated in oxidative degradation of AOII [15] and CAF. In the experiments on the oxidative degradation of CAF, 0.02 g of catalyst was dispersed in 100 mL of CAF solution in the presence of 22 mM H_2O_2 and stirred at 200 rpm for 4 hr at room temperature. At regular intervals, 5 mL of reaction suspension was withdrawn and filtered through a 0.2 μm filter syringe. The concentration of CAF supernatant solution was determined by high-performance liquid chromatography (HPLC) (Waters 2707 Autosampler) equipped with a XTERRA® RP18 column (4.6 mm \times 250 mm, 5 μm). The wavelength of photodiode array detector (PDA) was 275 nm for caffeine. The mobile phase was selected as methanol and ultrapure water (40/60; v/v) and the injection volume was 10 μL . The reaction was quenched by the addition of 50 μL of 1.0 M sodium thiosulfate ($\text{Na}_2\text{S}_2\text{O}_3$) into the CAF supernatant solution, prior to HPLC analysis.

The kinetic evaluation of oxidative degradation for both recalcitrant organics pollutants were investigated using pseudo-zero-order, first-order, second-order and BMG-Behnajady, Modirshahla, and Ghanbary [27] kinetic models. Pseudo-zero-order, first-order and second-order kinetic models are defined according to Eqs. (3)-(5), respectively:

$$C_t = C_o - k_o t \quad (3)$$

$$\ln C_t = \ln C_o - k_1 t \quad (4)$$

$$\frac{1}{C_t} = \frac{1}{C_o} + k_2 t \quad (5)$$

The k_o ($\text{mg L}^{-1} \text{min}^{-1}$), k_1 (min^{-1}), and k_2 ($\text{L mg}^{-1} \text{min}^{-1}$) are apparent kinetic rate constants of pseudo-zero-order, first-order, and second-order models, respectively, t is reaction time, and C_t is the pollutant concentration at a given time t .

The BMG model is written as in Eq. (6):

$$\left[1 - \left(\frac{C_t}{C_o} \right) \right]^t = m + bt \quad (6)$$

Where m and b are two constants respecting to initial oxidation capacities and reaction kinetics, respectively [27].

3. Results and discussion

3.1. Catalytic performances and kinetic analysis

Reactivity of CaMFeO_3 ($M = \text{Cu, Mo, Co}$) perovskite catalysts in the oxidation of acid orange II (AOII) macropollutant has been investigated in our previous works [15]. The AOII degradation data is summarized in TABLE 1. From TABLE 1, it was found that CaCuFeO_3 exhibited the most effective AOII degradation, with a rate of 97%, followed by CaMoFeO_3 at

90%, CaFeO_3 at 64%, and CaCoFeO_3 at 40%, within 60 min reaction time in the presence of H_2O_2 . Such finding reveals that the enhanced AOII degradation in the presence of CaCuFeO_3 perovskite catalyst during catalysis was attributed to the facile generation of $\cdot\text{OH}$ radicals due to fast redox cycling of active sites ($\equiv\text{Cu}^+/\equiv\text{Cu}^{2+}$ and $\equiv\text{Fe}^{2+}/\equiv\text{Fe}^{3+}$). The fast redox cycling of the active sites can be well correlated with the magnitude resistance of the electron transfer mobility during catalysis. Interestingly, the magnitude of the resistance for CaCuFeO_3 was the lowest ($\sim 404 \Omega$) compared to others substituted perovskite catalysts as reported elsewhere [15].

TABLE 1

Data of AOII degradation in presence of CaFeO_3 , CaCuFeO_3 , CaMoFeO_3 and CaCoFeO_3 perovskite catalysts

Catalyst	Degraded AOII at 60 min		
	Absorbance	$C_{\text{AOII},t}$ (mg/L)	AOII degradation (%)
CaFeO_3	0.5566	12.18	64%
CaCoFeO_3	0.9427	20.63	40%
CaMoFeO_3	0.1534	3.36	90%
CaCuFeO_3	0.0457	1.00	97%

Note: Experimental conditions: $C_{\text{AOII},0} = 35 \text{ mg L}^{-1}$; $\text{H}_2\text{O}_2 = 22 \text{ mM}$; Catalyst = 1.0 g L^{-1} ; and unadjusted pH solution. Calibration curve: $\text{Abs} = 0.0457 C_{\text{AOII}}$, $R^2 = 0.9998$

In this study, the catalytic performances of CaMFeO_3 ($M = \text{Cu, Mo, Co}$) perovskite catalysts were tested for CAF micropollutant and the degradation profiles are shown in Fig. 1. Similar catalyst's reactivity trend was also observed for CAF degradation in the presence of H_2O_2 . The catalyst's reactivity are as follows: CaCuFeO_3 (36%) > CaCoFeO_3 (24%) > CaMoFeO_3 (15%) > CaFeO_3 (10%). It was found that, after 60 min of reaction, CaFeO_3 perovskite catalyst was found to be completely deactivated, while the catalytic activity of both CaMoFeO_3 and

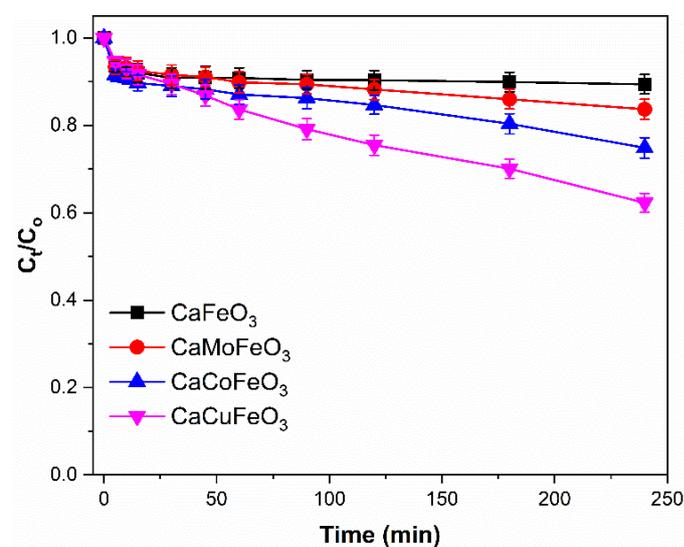


Fig. 1. Degradation profile of CAF in presence of CaFeO_3 , CaCuFeO_3 , CaMoFeO_3 and CaCoFeO_3 perovskite catalyst. Experimental conditions: CAF = 10 mg L^{-1} ; $\text{H}_2\text{O}_2 = 22 \text{ mM}$; Catalyst = 0.2 g L^{-1} ; unadjusted pH and $T = 27^\circ\text{C}$

CaCoFeO₃ were started to slowly deactivate until 4hr of catalysis. In contrast, CaCuFeO₃ was able to sustain its reactivity throughout the 4 hr of catalysis until it reached 36% degradation. Such findings suggest the efficient generation of [•]OH radicals facilitated by the regeneration of active site (=Cu⁺ and =Fe²⁺) during catalysis. The effective redox cycles between ≡Fe²⁺/≡Cu⁺ and ≡Fe³⁺/≡Cu²⁺ promote the efficient generation of [•]OH radicals, resulting in a much higher rate of CAF removal. It is interesting to note that the catalytic performance of CaCuFeO₃ in this work surpassed the CAF degradation reported by Simsek et. al [28] using LaFeO₃ perovskite catalyst and H₂O₂ as oxidant during dark catalysis.

Fig. 2 shows the chromatogram of CAF degradation in the presence of CaMFeO₃ (M = Cu, Mo, Co) perovskite catalysts at different reaction time. The chromatogram peak area appeared at retention time (RT) of 4.17 min represents the quantity or the concentration of CAF in the solution. The CAF chromatogram peak area decreased in the sequence of CaFeO₃ > CaMoFeO₃ > CaCoFeO₃ > CaCuFeO₃ at 4hr of reaction, which proved the CAF degradation profile as displayed in Fig. 1. The chromato-

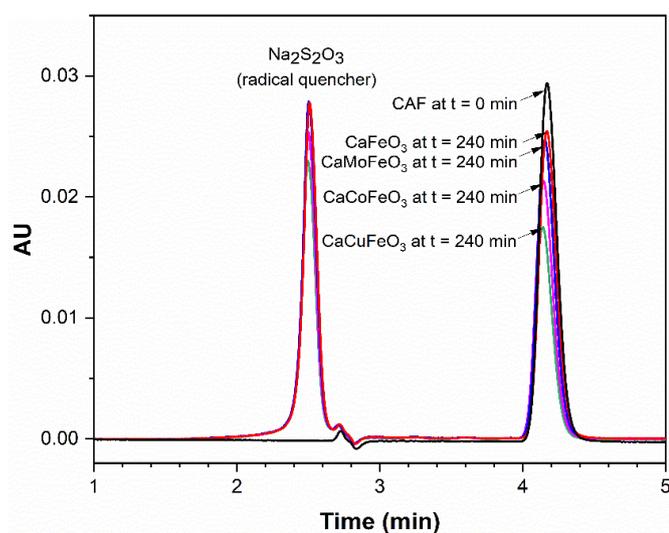


Fig. 2. Chromatogram of CAF during oxidative degradation using CaFeO₃, CaCuFeO₃, CaMoFeO₃ and CaCoFeO₃ at 4 hr of reaction time. Experimental conditions: CAF = 10 mg L⁻¹; H₂O₂ = 22 mM; Catalyst = 0.2 g L⁻¹; unadjusted pH and T = 27°C

gram peak at RT of 2.503 min indicates the presence of Na₂S₂O₃ as radical quencher to stop the reaction prior to HPLC analysis.

The kinetics behaviors of both AOII (Fig. 3) and CAF oxidation (Fig. 4) by CaMFeO₃ (M = Cu, Mo, Co) perovskite catalysts at unadjusted pH were further analyzed using four kinetic models (pseudo-zero-order, first-order, second-order and BMG). The results of correlation coefficients (*R*²), apparent kinetic constants of the pseudo-zero-order, first-order, second-order (*k*₀, *k*₁ and *k*₂) and kinetics' parameters obtained on the BMG model (1/*m* and 1/*b*) for both AOII and CAF oxidation are shown in TABLE 2. As illustrated in TABLE 2, the pseudo-second order kinetic model fitted well to the AOII oxidation by all CaMFeO₃ (M = Cu, Mo, Co) perovskite catalysts, as it obtained higher *R*² values than the zero-order, first-order and BMG kinetic models. On the contrary, distinctive kinetic behavior was observed in the oxidative degradation of CAF. Only CaCuFeO₃ followed the pseudo-first order kinetic model, whereas CaFeO₃, CaMoFeO₃ and CaCoFeO₃ conformed to the BMG kinetic model. This result indicates that the degradation kinetics of heterogeneous catalysis was mainly influenced by the nature of recalcitrant organic pollutant in presence of perovskite catalyst.

For instance, the kinetic behavior profile of the CaCuFeO₃ perovskite catalyst showed a dependence on the molecular size and the dissociation constant (*pK_a*) of the recalcitrant organic pollutant. The oxidative degradation of the macropollutant (AOII dye) can be well described by the pseudo-second-order kinetic model, while the pseudo-first-order kinetic model applies to the micropollutant (CAF) (Fig. 5). The *pK_a* value of AOII and CAF is 11.4 [29] and 10.4 [30], respectively. These molecules are present in neutral or protonated form when pH of the solution is lower than the *pK_a* [31]. At the unadjusted pH of reaction mixture (pH 6.4), AOII molecules (1.25-1.27 nm [32]) tend to dissociate by deprotonation of the -NH=N= groups due to weak acidic strength [29], which subsequently leads to electrostatic repulsion between AOII and the negative-charge of CaCuFeO₃ perovskite catalyst [15]. Therefore, the oxidative degradation of AOII is likely associated with a possible combination of interactions [29] between the concentration of oxidant (H₂O₂) to be activated into [•]OH radicals and the concentration of AOII during heterogeneous catalysis. This interaction is

TABLE 2

Apparent kinetic rate constants of the zero-order (*k*₀), first-order (*k*₁), and second-order (*k*₂), kinetics' parameters obtained on the BMG model (1/*m* and 1/*b*) and correlation coefficients (*R*²) obtained after data fits for AOII (60 min) and CAF (4 hr) oxidation

Pollutant	Catalyst	Zero Order		First Order		Second Order		BMG				
		<i>k</i> ₀ (mg L ⁻¹ min ⁻¹)	<i>R</i> ²	<i>k</i> ₁ (min ⁻¹)	<i>R</i> ²	<i>k</i> ₂ (L mg ⁻¹ min ⁻¹)	<i>R</i> ²	<i>m</i>	1/ <i>m</i> (min ⁻¹)	<i>b</i>	1/ <i>b</i>	<i>R</i> ²
AOII	CaFeO ₃	0.3238	0.8766	0.0161	0.9629	0.0009	0.9920	17.6056	0.0568	1.3770	0.7262	0.9181
	CaMoFeO ₃	0.3957	0.6083	0.0359	0.8690	0.0045	0.9937	4.5475	0.2199	1.0472	0.9549	0.9908
	CaCoCoO ₃	0.2031	0.8580	0.0077	0.9109	0.0003	0.9221	27.6243	0.0362	2.2272	0.4490	0.9205
	CaCuFeO ₃	0.4942	0.6755	0.0613	0.9012	0.0192	0.9254	2.0404	0.4901	0.9996	1.0004	0.9236
CAF	CaFeO ₃	0.0022	0.6596	0.0002	0.7723	0.00003	0.7852	238.0952	0.0042	9.6805	0.1033	0.9944
	CaMoFeO ₃	0.0045	0.7304	0.0005	0.7863	0.00005	0.8211	153.8462	0.0065	6.3412	0.1577	0.9450
	CaCoCoO ₃	0.0073	0.8314	0.0008	0.8624	0.00010	0.8880	128.2051	0.0078	4.1929	0.2385	0.9167
	CaCuFeO ₃	0.0141	0.9565	0.0018	0.9930	0.00020	0.9910	59.88024	0.0167	2.4160	0.4139	0.8398

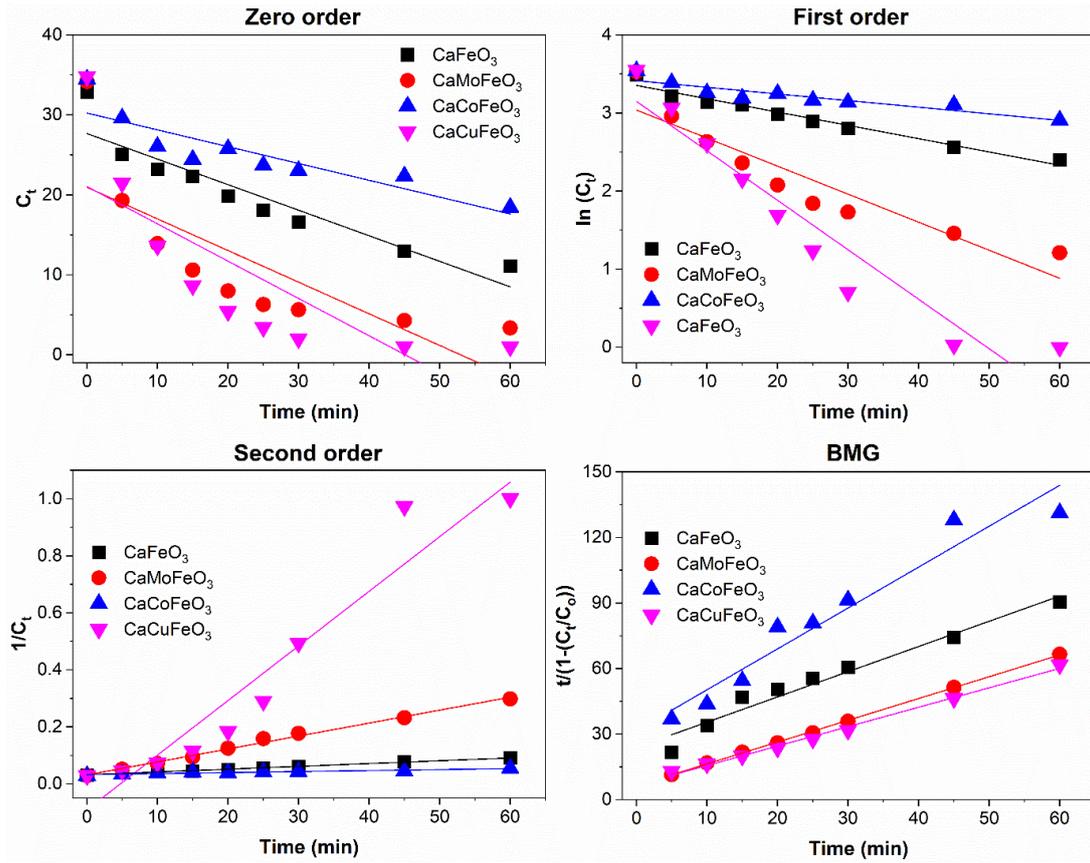


Fig. 3. AOII oxidative degradation in presence of B-site substituted CaMFeO_3 (M = Mo, Co, Cu) perovskite catalysts using different kinetic models. Experimental conditions: AOII = 35 mg L⁻¹; H₂O₂ = 22 mM; Catalyst = 1.0 g L⁻¹; unadjusted pH and T = 27°C

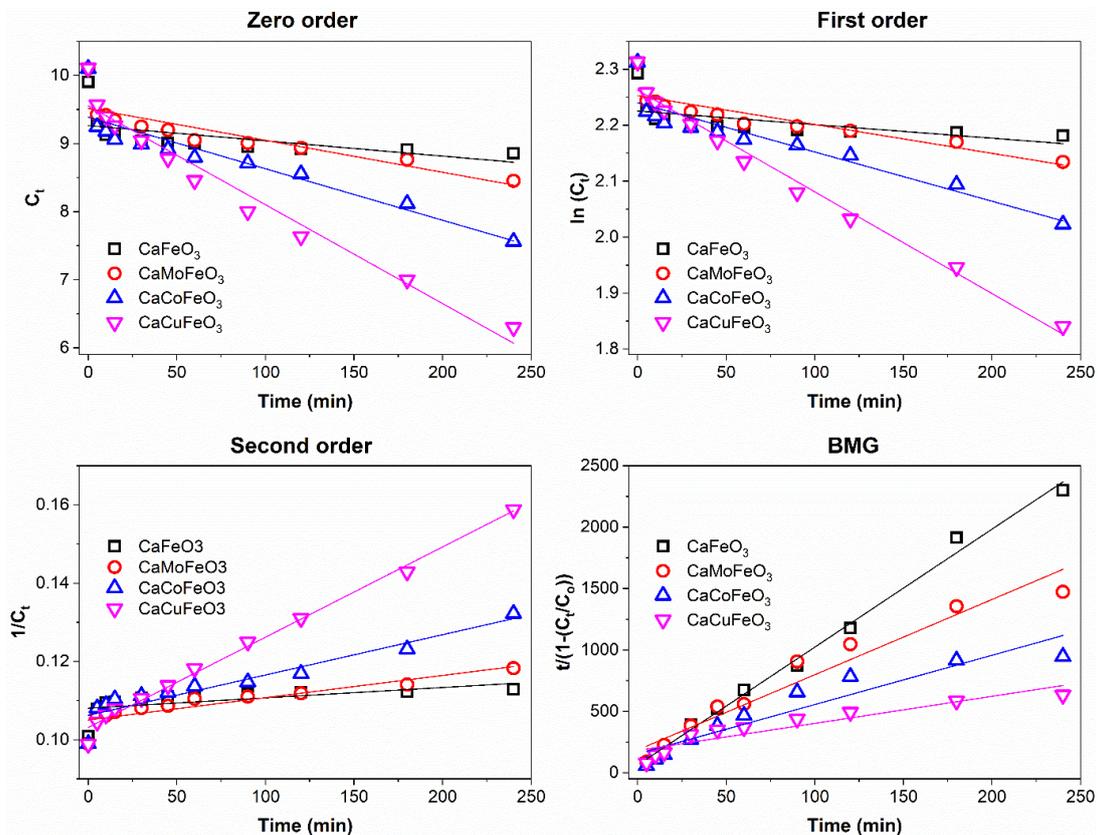


Fig. 4. CAF oxidative degradation in presence of B-site substituted CaMFeO_3 (M = Mo, Co, Cu) perovskite catalysts using different kinetic models. Experimental conditions: CAF = 10 mg L⁻¹; H₂O₂ = 22 mM; Catalyst = 0.2 g L⁻¹; unadjusted pH and T = 27°C

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